

My Calculation

Engineering Calculation Sheet

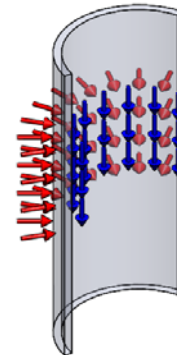
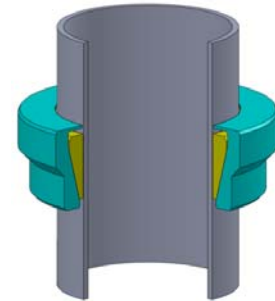
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Calculation No 006

Subject Reinhold-Spiri formula derivation based on axisymmetric radial load on pipe lateral surface Prepared By YUDHI Date 9-Oct-15

This calculation was conducted in order to verify Reinhold-Spiri formula as a slip crushing load (F_z) based on axisymmetric wedge that generates axisymmetric radial load on pipe lateral surface. As the wedge slip bite on pipe, pipe shall be exposed to radial load. By using Lamé equation for a thick wall cylinders, the axial and hoop stress on pipe ID can be estimated from radial stress acting on pipe OD. since radial stress as a function of axial load, the axial load at which VME stress at pipe ID reaches stress to cause pipe yielding can be determined.

Nomenclature

| | |
|--------------|--|
| OD | Pipe outer diameter |
| ID | Pipe inner diameter |
| A_1 | Pipe cross section area |
| A_L | Pipe lateral surface area around slip bite |
| S_y | Pipe yield material based on grade |
| F_A | Pipe axial load |
| F_R | Pipe radial load |
| | |
| L | Slip length |
| α | Slip angle |
| μ | Friction coefficient |
| | |
| S_a | Axial stress |
| $S_{r(o/i)}$ | Radial stress (outer / inner) |
| S_h | Hoop stress |
| K | Transverse factor from axial stress (S_a) to radial stress (S_r) |
| F_z | Slip crushing load |



Let

$$S_{ro} = (K A_1 / A_L) S_a \quad \text{--- see page 2 for transverse factor derivation}$$

From Lamé equation for thick wall cylinder ($S_{ri} = 0$ as radial stress on pipe ID vanish)

$$\begin{aligned} S_h &= \left[\frac{(OD^2 + ID^2)}{(OD^2 - ID^2)} S_{ri} - \frac{2OD^2}{(OD^2 - ID^2)} S_{ro} \right] \quad \text{--- [1]} \\ &= - \frac{2OD^2}{(OD^2 - ID^2)} S_{ro} \\ &= - \frac{2OD^2}{(OD^2 - ID^2)} [(K A_1 / A_L) S_a] \end{aligned}$$

Apply VME stress equivalent on pipe ID.

$$\begin{aligned} S_y &= \left\{ \left[(S_a - S_{ri})^2 + (S_{ri} - S_h)^2 + (S_h - S_a)^2 \right] / 2 \right\}^{0.5} \\ &= \left\{ \left[(S_a)^2 + (S_h)^2 + (S_h - S_a)^2 \right] / 2 \right\}^{0.5} \\ &= \left\{ \left[(S_a)^2 + (- \frac{2OD^2}{(OD^2 - ID^2)} S_{ro})^2 + (- \frac{2OD^2}{(OD^2 - ID^2)} S_{ro} - S_a)^2 \right] / 2 \right\}^{0.5} \\ &= \left\{ \left[(S_a)^2 + [- \frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) S_a]^2 + (- \frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) S_a - S_a)^2 \right] / 2 \right\}^{0.5} \\ &= \left\{ \left[(S_a)^2 + [- \frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) S_a]^2 + (- \frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) S_a - S_a)^2 \right] / 2 \right\}^{0.5} \\ &= \left\{ S_a^2 \left[1 + \left[\frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) \right]^2 + \left[\frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) + 1 \right]^2 \right] / 2 \right\}^{0.5} \\ &= S_a \left\{ \left[1 + \left[\frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) \right]^2 + \left[1 + \frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) \right]^2 \right] / 2 \right\}^{0.5} \\ &= (F_z / A_1) \left\{ \left[1 + \left[\frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) \right]^2 + \left[1 + \frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) \right]^2 \right] / 2 \right\}^{0.5} \end{aligned}$$

$$F_z = (S_y \cdot A_1) \left\{ 2 \left[1 + \left[\frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) \right]^2 + \left[1 + \frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) \right]^2 \right] \right\}^{0.5}$$

since

$$A_1 = \pi/4 (OD^2 - ID^2)$$

$$A_L = \pi OD L$$

$$\begin{aligned} F_z &= (S_y \cdot A_1) \left\{ 2 \left[1 + \left[\frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) \right]^2 + \left[1 + \frac{2OD^2}{(OD^2 - ID^2)} (K A_1 / A_L) \right]^2 \right] \right\}^{0.5} \\ &= (S_y \cdot A_1) \left\{ 2 \left[1 + \left[\frac{K OD}{2L} \right]^2 + \left[1 + \left(\frac{K OD}{2L} \right)^2 \right] \right] \right\}^{0.5} \quad \text{--- [2]} \end{aligned}$$

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Transverse factor derivation

Free body diagram determination

$$F_R + R_1 + \mu R_1 + F_A = 0$$

$$F_A = R_1 \cdot \sin \alpha + \mu R_1 \cdot \cos \alpha \quad \text{---} \quad \text{for } \Sigma F_Y = 0$$

$$R_1 \cdot \cos \alpha = F_R + \mu R_1 \cdot \sin \alpha \quad \text{---} \quad \text{for } \Sigma F_X = 0$$

$$F_R = R_1 \cdot \cos \alpha - \mu \cdot R_1 \cdot \sin \alpha$$

$$= R_1 \cdot (\cos \alpha - \mu \cdot \sin \alpha)$$

$$R_1 = F_R / (\cos \alpha - \mu \cdot \sin \alpha)$$

$$F_A = R_1 \cdot \sin \alpha + (\mu \cdot R_1) \cdot \cos \alpha$$

$$= R_1 \cdot (\sin \alpha + \mu \cdot \cos \alpha)$$

$$= [F_R / (\cos \alpha - \mu \cdot \sin \alpha)] (\sin \alpha + \mu \cdot \cos \alpha)$$

$$= F_R [(\sin \alpha + \mu \cdot \cos \alpha) / (\cos \alpha - \mu \cdot \sin \alpha)]$$

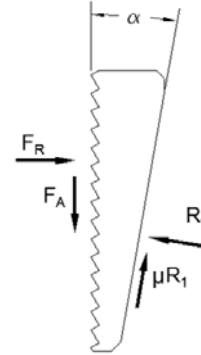
$$= F_R / \cot(\alpha + \theta)$$

--- [4] page 157

$$F_R = F_A \cdot \cot(\alpha + \theta)$$

--- $\cot(\alpha + \theta)$ known as transverse factor from pipe axial load to radial load [2]

$$F_R = F_A \cdot K$$



Then

$$S_{ro} \cdot A_L = K \cdot S_a \cdot A_1$$

$$S_{ro} = (K A_1 / A_L) S_a$$

Reference:

- [1] SPE 13434 - Triaxial Load Capacity Diagrams Provide a New Approach to Casing and Tubing Design Analysis
- [2] SPE 99074 - A Re-examination fo Drillpipe/Slip Mechanism
- [3] SPE 80169 - Advanced Slip Crushing Consideration for Deepwater Drilling
- [4] Machinery Handbook, 27TH Edition